

Equation (13b) may now be re-written thus

$$p_c = \alpha \sigma_{00} e^{-\chi T} - \left\{ \frac{16G\gamma'}{\pi(1-\nu)k_0 e^{-\epsilon T}} - \alpha k_0 e^{-\epsilon T} \right\} d^{-\frac{1}{2}}.$$

Eliminating constants, this becomes

$$p_c = \xi e^{-\chi T} - (\zeta e^{\epsilon T} - \lambda e^{-\epsilon T}) d^{-\frac{1}{2}} \quad (17)$$

where

$$\xi = \alpha \sigma_{00}, \quad \zeta = \frac{16G\gamma'}{\pi(1-\nu)k_0} \text{ and } \lambda = \alpha k_0.$$

Expanding equation (17) and ignoring second order terms (χ and ϵ are both small), we get

$$p_c = \xi(1 - \chi T) - \{\zeta(1 + \epsilon T) - \lambda(1 - \epsilon T)\} d^{-\frac{1}{2}}$$

or

$$p_c = \xi - (\zeta - \lambda)d^{-\frac{1}{2}} - \xi\chi T - \epsilon(\zeta + \lambda)d^{-\frac{1}{2}}T. \quad (18)$$

For constant grain size, this reduces to Pugh's⁽³⁾ equation (2) with

$$A' = \frac{\xi - (\zeta - \lambda)d^{-\frac{1}{2}}}{\xi\chi + \epsilon(\zeta + \lambda)d^{-\frac{1}{2}}}$$

$$B' = \frac{1}{\xi\chi + \epsilon(\zeta + \lambda)d^{-\frac{1}{2}}}$$

5. CONCLUSIONS

A theory for the brittle-ductile transition pressure has been developed and applied to the transition in zinc. It is shown that the quantities involved are of the right order. The theory predicts that the transition pressure increases both with σ_0 the frictional stress opposing the motion of a free dislocation (which may be increased by strain or quench-ageing and irradiation damage) and with increasing grain size.

The effect of temperature on the transition pressure is shown to be consistent with the empirical relationships of Pugh^(1,3) and Galli and Gibbs⁽²⁾.

REFERENCES

1. PUGH, H. Ll. D. The mechanical properties and deformation characteristics of metals and alloys under pressure. *NEL Report* No 142. East Kilbride, Glasgow: National Engineering Laboratory, 1964.
2. GALLI, J. R. and GIBBS, P. The effect of hydrostatic pressure on the ductile-brittle transition in molybdenum. *Acta Metall.*, 1964, 12, 775-778.
3. PUGH, H. Ll. D. Recent developments in cold forming. *In Bulleid Memorial Lectures*, Vol IIIB. Nottingham: University of Nottingham, 1965.
4. PETCH, N. J. The transition temperature in notched specimens. *In* MARSH, W. D. *Brittleness of Metals*. Proc. Conf. held in Culcheth, 1957, pp 3-17. *UKAEA IG Report* 145(RD/C). London: H.M. Stationery Office, 1958.

5. COTTRELL, A. H. Theory of brittle fracture in steel and its application to radiation embrittlement. In MARSH, W. D. Brittleness in Metals. Proc. Conf. held in Culcheth, 1957, pp 18-20. UKAEA IG Report 145(RD/C). London: H.M. Stationery Office, 1958.
6. PETCH, N. J. Ductile-brittle transition in fracture of α iron-1. *Phil. Mag.*, Series 8, 1958, 3(34), 1089-1097.
7. STROH, A. N. Formation of cracks as a result of plastic flow. *Proc. R. Soc.*, Series A, 1954, 223(1154), 404-414.
8. STROH, A. N. The formation of cracks in plastic flow, II. *Proc. R. Soc.*, 1955, 232(1191), 548-560.
9. SACK, R. A. Extension of Griffith's theory of rupture to three dimensions. *Proc. Phys. Soc.*, London, 1946, 58, 729-736.
10. ESHELBY, J. D., FRANK, F. C. and NABARRO, F. R. N. The equilibrium of linear arrays by dislocations. *Phil. Mag.*, 1951, 42(327), 351-364.
11. ARMSTRONG, R., CODD, I., DOWTHWAITE, R. M. and PETCH, N. J. Plastic deformation of polycrystalline aggregates. *Phil. Mag.*, 1962, 7(73), 45-48.
12. HESLOP, J. and PETCH, N. J. The stress to move a free dislocation in alpha iron. *Phil. Mag.*, Series 8, 1956, 1, 866-873.

LIST OF FIGURES

1. The formation of a crack.